### **DAFTAR LAMPIRAN**

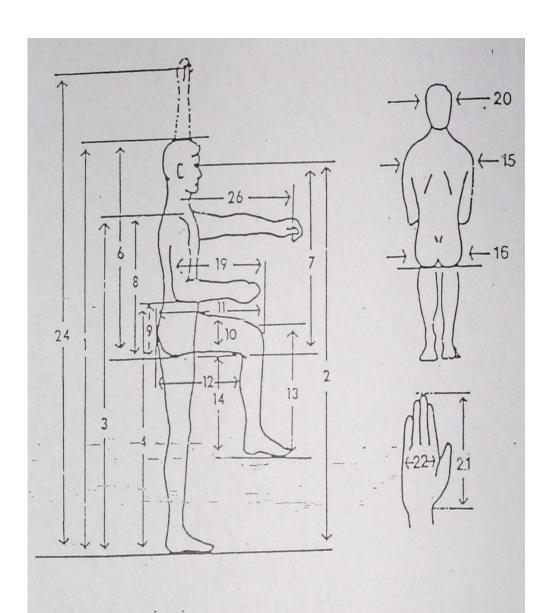
Lampiran	Judul	Halaman
1	Data Antropometri Orang Indonesia	L – 1
1	Gambar Pengukuran Antropometri	L-2
2	Illumination Level For Interior Lighting	L-1
2	Reflectance Factor For Surface Color	L-2
2	Thermal Comfort Zone	L-3
2	Exposure to Noise	L-5
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2	Penentuan Jumlah Lampu	L-7

Tabel 5.3

Antropometri masyarakat Indonesia yang didapat dari interpolasi masyarakat British dan Hongkong (Pheasant, 1986) terhadap masyarakat Indonesia (Suma'mur, 1989) serta istilah dimensionalnya dari (Nurmianto, 1991a ;Nurmianto, 1991b).

Dimana : G<sub>x</sub> = nilai rata-rata (mean), T = nilai standar deviasi (SD), 5% = nilai 5 persentil, 95% = nilai 95 persentil

DIMENSI TUBUH		P	RIA			WAN	ITA	
D1.112131 10301.	5%	X	95%	0.2	3%	X	95% -	S.D
1. Tinggi Tubuh Posai berdiri Tegak	1.532	1.632	1.732	61	1.464	1.563	1.662	60
2. Tinggi Mua	1.425	1.520	1.615	58	1.350	1.446	1.542	58
5. Tinggi Bahu	1.247	1.338	1.429	55	1.184	1.272	1.351	54
4. Tingri Siku	932	1.003	1.074	43	886	957	1.028	- 43
5. Tinggi Gengganuu Tangan (Kauckle) pada Posisi Relaks kebawah	655	718	782	39	645	708	771	38
6. Tinggi Budan pada Posisi Duduk	809	864	919	33	775	834	893	36
7. Tinggi Mata pada Posisi Duduk	69-i	749	804	33	666	721	776	53
8. Tinggi Bahu pada Posisi Dudul-	523	572	621	30	501	550	599	30
9. Tinggi siku pada Posisi _ Duduk	181	231	282	31	175	229	283	33
10. Tebal Paha	117	140	163	14	115	140	165	15
11. Jarak dari Pantat ke Lutut	500	545	590 -	27	488	537	586	30
(poplited) ke Pantit	405	450	495	27	488	537	586	30
5. Tinggi Lutut	448	496	544	29	428	472	516	27
4. Tinggi Lipat Lutter (popli- teal)	36 i	403	445	26	337	382	428	28
5. Lebar Bahu (bidekoid)	382	424	466	26	342	385	428	26
6. Leber Punggul	291	331	371	24	298	345	392	29
7. Tebul Dada	174 !	212	250	23	178	228	278	30
8. Tebul Perus (abdominal) .	174	229	282	33	175	231	287	34
9. Jarok dari Siku ke Ujung Jari	405	439	473	21	374	409	287	34
U. Lebar Kepala	140	150	160	6	135	146	157	7
1. Panjang Tangan	161	176	191	9	153	168	183	9
2 Lebar Taugan	71	79	87	5	64	71	78	4
3. Jarak Bentang dari Ujung Jari Tangan Kiri ke Kanan	1.520	1.663	1.806	87	1.400	1,523	1.646	75
Tinggi Pegangan Tangan     (grip) pada Posisi Tangan     Vertikal ke Atas & Berdiri Tegak	1 795	1.923	2.051	78	1.713	1.841	1.969	79
(grip) pada Ponu Tangan Vertikal ke Atas & Dudni	1.065	1 169	1.273	63	945	1.030	1.115	52
(grip) ke Punggunan Tangan (grip) ke Punggung pada Potisi Tangan ke Gepan (horisontal)	649	tos	707	37	G10	661	712	31



Gambar 5.2a.

Anthropometri tubuh manusia yang diukur dimensinya.

Sumber data: Stevenson, 1989 : Nurmianto, 1991)

## Table WRKSTN-D5: Recommended Illumination Levels for Interior Lighting<sup>12</sup>

Activity type	Dlumination level (lx)
Rough orientation	75
Occasional rough visual tasks	150
Rough assembly	320
Rough toolmaking	550
Office work—simple	750
Bookkeeping-small character size	1,500
Difficult inspection	1,500
Technical drawing	2,200
Precise assembly work	5,000
Prolonged difficult visual task	7,500
Precise and delicate visual work	11,000
Very special visual tasks—extremely low contrast and small object size	15,000

# Table WRKSTN-D6: General Illumination Levels and Types of Illumination for Different Task Conditions<sup>3</sup>

Task condition	Type of task or area	Illuminance level (Ftc)	Type of illumination
Small detail, low con- trast, prolonged peri- ods, high speed, ex- treme accuracy.	Sewing, inspecting dark materials, etc.	100	General plus supple- mentary, e.g., desk lamp.
Small detail, fair contrast, speed not essential.	Machining, detail draft- ing, watch repairing, inspecting medium ma- terials, etc.	50-100	General plus supple- mentary.
Normal detail, prolonged periods.	Reading, parts assembly; general office and lab- oratory work	20-50	General, e.g., over- head ceiling fixture.
Normal detail, no pro- longed periods.	Washrooms, power plants, waiting rooms, kitchens	10-20	General, e.g., random natural or artificial light
Good contrast, fairly large objects.	Recreational facilities	5-10	General.
Large objects	Restaurants, stairways, bulk-supply ware- bouses.	2-5	General.

### Table WRKSTN-D7: Reflectance Factors for Surface Culor3

Color	Hellectance	Color	Reference
White	85		
Light: Cream Gray- Yellow Buff Green Blue	75 75 75 70 65 55	Dark: Gray Red Brown Blue Green	30 13 10 8 7
Modium: YeBo= Buf. Gray Gray. Blue.	65 63 55 52 33	Wood Finish: Maple Satin wood Englieb Oak Walnut Mahogany	42 34 17 18 12

### Table WRKSTN-D8: Techniques for Controlling Glare4

To Control Direct Glare	To Control Indirect Glare (Veiling Reflections and Reflected Glare)
Position luminaires, the lighting units, as far from the operator's line of sight as is practical	Avoid placing luminaires in the indi- rect-glare offending zone (see Figure VC-2)
Use several low-intensity luminaires in- steed of one bright one	Use luminalities with diffusing or polar- izing lenses
Use luminaires that produce a betweing light distribution, and position workers so that the highest light level	Use surfaces that diffuse light, such as flat paint, non-gloss paper, and tax-tured finishes
comes from the sides, not front and back	Change the orientation of a work- place, task, viewing angle, or viewing

Use luminaires with louvers or prismatic lenses

Use indirect lighting

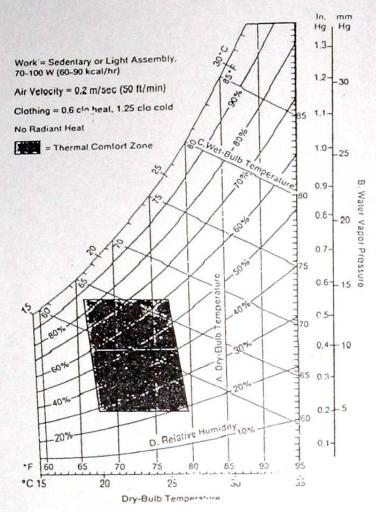
Use light shields, hoods, and visors at the workplace it other methods are impractical

direction until maximum visibility is

\* The effectiveness of the batwing distribution veries with the orientation of the workplace and worker, it can also be used to control indirect glare, because maximum output is in the arc between approximately 35" to 45" angles.

achieved

Examples of ways to control direct glare (column 1) and indirect glare (column 2) at the workplace are given. These methods include design approaches that can be used when installing the lighting, as well as interventions that can be made after glare has been identified in a workplace.



The dry bulb temperature and humidity combinations that are comfortable for most nearly defined by the bulb temperature range is from 19° to 26°C (66° 79°F), and relative humidities (shown as parallel curves) range from 20 to 85 per cent, with 35 to 65 percent being the most common values in the comfort zone. On this chart ambient dry bulb temperature (A) is plotted on the horizontal axis are indicated as parallel vertical lines; water vapor pressure (B) is on the vertical axis. Wet bulb temperatures (C) are shown as parallel lines with a negative slope; the intersect the dry bulb temperature lines and relative humidity curves (D) on the chart. In the definition of the thermal comfort zone, assumptions were made about the work load, air velocity, radiant heat, and clothing insulation levels. The assumptions are given in the top left corner of the chart.

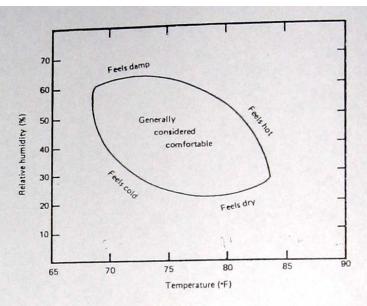


Figure WRKSTN-E4: Comfort Zone as a Function of Relative Humidity Versus Temperature<sup>2</sup>

Table WRKSTN-E3: Maximum Recommended Work Loads, Heat Discomfort Zone<sup>1</sup>

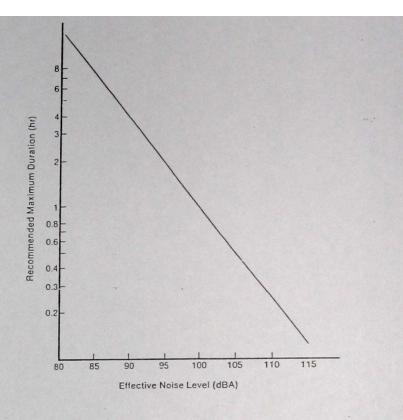
	Maximu	m Recomi	nended W	ork Load	
Ambie	nt		Relative	Humidity	
Tempe	erature				
°C	°F	20%	40%	60%	80%
27	80	VH	VH	VH .	Н
32	90	VH	Н	M	L
38	100	Н	M	L	NR
43	110	М	L	NR	NR
49	120	L	NR	NR	NR

Note: Assumptions include 2-hour continuous exposure, 0.6 clo insulation, air velocity less than 0.5 m/sec (100 ft/min). Higher work loads may be sustained for shorter work periods. See Figure VD-3 for further information. Definitions of work load abbreviations: VH = very heavy, 350-420 W (300-360 kcal/hr); H = heavy, 280-350 W (240-300 kcal/hr); M = moderate, 140-280 W (120-240 kcal/hr); L = light, less than 140 W (120 kcal/hr), NR = not recommended for 2 hours of continuous exposure.

### EXPOSURE TO NOISE

# Table WRKSTN-E9: Intensity and Effects of Common Noises <sup>2</sup>

Common Sounds	Noise Level (dB)	Effect
Carrier deck jet operation Air raid siren	140	Painfully loud (blurring vision, nausea, dizziness)
Jet takeoff (200 feet) Thunderclap	130	Begin to "feel" the sound
Loud Disco Auto horn (3 feet)	120	Hearing becomes uncomfortable
Pile drivers	110	Cannot speak over the sound
Garbage truck	100	
Heavy truck (50 feet) City traffic	90	Very annoying
Alarm clock (2 feet) Hair dryer	80	Annoying
Noisy restaurant Freeway traffic Man's voice (3 feet)	70	Telephone use difficult
Air conditioning unic	60	Intrusive
Light auto traffic (100 feet)	50	Ouiet
Living room Bedroom Quiet office	40	
Library Soft whisper (15 feet)	30	Very quiet
Broadcasting studio	20	
	10	Just audible
	0	Hearing begins



The recommended maximum duration of exposure (in hours, hr, on the vertical axis) to noise of different intensities (in decibels, dBA, on the horizontal axis) is given. The higher the noise level, the less time a person should be exposed to it in order to reduce the risk of hearing damage. Noise levels above 115 dBA should be avoided; levels below 80 dBA are not known to contribute to hearing loss over extended exposure times.

Figure WRKSTN-E7: Guidelines for Noise Exposure to Protect Hearing; Recommended Maximum Duration Versus Noise Level<sup>1</sup>

TABLE 20.2 Coefficients of Utilization for Typical Lundingiess with Suggested Maximum Spacing Ratios

To obtain a coefficient of utilization:

1. Determine cavity taxos for the name, ceiling, and these,

Determine the effective ceiling and flust cavity refectioner from Table 20.1. Use initial ceiling, flust, and wall reflectances.
 Obtain exefficient of origination (CU) for 20th effective than enemy reflective ceiling cavity refectioners above and below reflections inheritance in sign. In order 20.

interpolate between these CUs to obtain CU for arth 2 celling chairs between the paying chairs and between these colds to obtain CU for arth 2 celling chairs of the checker.

1. If effective floor castly retherance differs a gainfandly from 20%, choin withplier from Table 204 and apply this in the CU dualised to asking castly retherance (p<sub>1</sub>, 1 of 30° celling), and application for exact hypers are 163 Hundreak (10%), in whitely the light of p<sub>2</sub> = 30° km 0 83 and 0.36, respectively. This is an approximation. For exact hypers are 163 Hundreak (10%),

3. Use the figure in the last column (p<sub>1</sub>, c = 0; p<sub>2</sub> = 0) for overliced tybing, i.e., no walls or celling.

per = pateers effective cesting cavity reflectance

P. " perten wall reflectance

RCR = mineravity ratio

Maxinum SIMH guide = sain of maximum luminaire species in insuning above surt plane.

HARD. IN SETTO CARE, INTRIBUTE DATA IN this LIDE ARE POSSED FOR AN ACTUAL SPIRES, IN COLOR CARES, THE CARES, THE CONTRACTE OF EXECUTE OF ASSEDING THE STATE OF ASSEDING THE SPIRES OF ASSEDING WHEN ASSEDING THE STATE OF ASSEDING THE ASSEDING THE STATE OF ASSEDING THE ASSEDING T

	I Voical Distribution and	tion and	100					0					>
	Parcent Lamp Lumens	umans	Un' -	. 50	30	10	50	30	10	25	30	101	0
		Махітит						-	1			1	
	Maintenance	SIMH	0	See	llicient	10 01	(Filzan	Joj uc	20% €	Hech	e Floo	r Cavi	Coefficients of Utilization for 20%, Effective Floor Cavity Reflectance
ואסוכים רחשהים ו	Caregory	Cuiac	HCH			-			(brc =	20)			
	>	1.5	0	.87	.87	187	18.	18	81	69	69	69.	44.
			-	12.	.67	63	99.	62	.59	.58	.53	.50	16.
()=	_{		7	19	.54	91.	56	90	46	.47	.43	39	8
=	:	/		.52	.45	.39	£.	42	37	-5	38	.31	.18
	-	_	7	94.	.38	8	.42	38	.30	36	.30	.26	51.
		-	S	C. 4.	8	.27	.37	3	25	.32	35	.22	. 12
)	257	1	9	.36	.28	.23	.33	56	12	.28	.23	19	.10
	1		7	.32	25	20	.28	23	.18	.25	.20	.16	80'
Pendant diffusing sphere			90	.29	22	17	.27	20	91.	.23	117	14	70.
with incal'descent			61	.25	D)	. 15	.24	3.	14	.20	.15	. 12	80:
dms			10	.23	17	.13	22	3	.12	07.	14	.10	.05

8	57	.42	36	30	.25	21	.18	.15	.13	-	89	53	45	.35	82	.24	.20	11.	.15	.12	11.	.85	89	.56	94	39	33	.28	.24	.21	.18	-
.66	56	46	.38	.32	.27	183	.20	.17;	- 4-	.12	187	.67	54	44	.37	.31	.26	.23	61.	.17	. 15	1.0.1	.80	.65	.54	46	.38	.33	.28	.25	.21	101
99	57	48	14	36	.30	38	53	20	17	15	.87	.70	999	49	.42	.36	3	.27	.24	5	.19	1.0.1	.83	69	.59	25.	44	38	34	.30	.26	*
99.	59	15	45	40	35	.31	.28	.25	.22	.20	19	73	.63	.55	.48	.42	38	.34	3	15.	25	1.01	.87	.75	99.	.58	£2	97	- 4	.37	.33	4
69	57	47	36	3	27	23	83	.17	14	.12	8;	.73	3	.48	96.	33	.28	.24	5.	.18	91.	1.09	.85	.69	.57	48	04.	34	.30	.25	.22	
69	50	.50	43	.37	31	.27	24	.20	18	16	96	77	.63	53	.46	33	34	.29	.26	.23	.20	1.08	.89	.74	.63	.54	90.	040	.35	.3	.27	
63.	19.	53	47	41	36	32	23	25	23	20)	96	81	69	69	23	46	10	37	33	99	27	1 09	66	80	20	62	55	64.	44	39	35	**
.71	3	.47	36	.33	.27	.23	8	17	7	.12	1.01	17.	19	8	-4	K	83	25	57	.18	.16	1.13	.86	.70	58	O.	+	35	.30	.26	.22	1
7.	9.	ī,	43	.37	.32	27	24	2.5	.18	18	1.01	1810	99	.56	14.	7	35	.31	.23	.23	12.	1.13	36.	.76	.65	.55	74.	14.	.36	.32	.28	100
.7	.62	.55	.48	.42	.37	.33	53	2,	23	100	1.01	38.	R	3	8.	.49	43	39	34	6	28	1.13	96	.03	.73	79.	.56	50	45	940	36	
0	-	cu	0	4	2	9	7	80	5	2	0	-	Cz	~	4	2	3	~	(11)	6	10	0	-	2	3	4	3	9	1	c.	6	
٧ ١.7				1		- 1					1 1.6/1.2				中華		3					1 1.4/1.2				1		18.11 11				
No.	THE STATE OF THE S				000000000000000000000000000000000000000	dictabulation (and the	640 mm (20 may)	Oroman (2) wide	יייייייייייייייייייייייייייייייייייייי	liat prismatic 1908	5			( P. )	OK.	The state of the s				Two-lamp fluorescent	strip unit	49			R. C.				Iwo-lamp fluorescent	strip unil with 235"	reflector fluorescent	

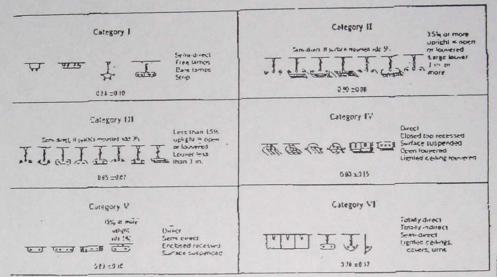


Fig. 20.36 The LOD factor is determined from the category of luminaire, which is an indication of its primeness to dirt accumulation, plus a knowledge of room ambient conditions.

ditions of din and maintenance. The categories correspond to those of the IES.

Total LLF is the product of all the depreciation factors above that is:

For example, a fluorescent air troffer in a regularly maintained group-lamp-replacement, air-conditioned office might typically have an LLF of

LLF = 
$$1.1 \times 1 \times 0.92 \times 1 \times 0.95$$
  
  $\times 0.9 \times 1.0 \times 0.93 = 0.80$ 

The same fixture in the same office, but with walls and fixture cleaned only when replacing borned-out lamps would typically have an f.f.F of

ULF = 1.1 × 1 × 0.92 × 1 × 0.87 
$$\bullet$$
  
× 0.85 × 0.95 × 0.75 = 0.55

Thus, if in the first case the maintained illumination is E fe, in the second case it is 0.25/0.80 or 0.69Efe, that is, a reduction of 31% as a result of poor maintenance. When a detailed determination of light loss factor is not possible, use the factors given in Section 20.33. They are somewhat more conservative than these given in Section 20.3c.

#### 20.31 Determination of Coefficient of Utilization (CU) by the Zonal Cavity Method

The coefficient of utilization connects a particular fixture to a particular space, by relating the lumunaim's right distribution characteristic to tile from size and its surface reflectances. To account for the luminaire's mounting height and its relationship to the working plane, the space is divided into three cavities: the ceiling cavity above the fixture, the Boor cavity below the working plane. and the axin cavity between the two (see Fig. 20.37) Given the surface reflectances, the effective reflectances of the floor and ceiling exerties can be obtained. With these, the CU can be selected from the tables (either Table 20.2 or manufacturer's data) and the lumen formula (equation 20.3 above) applied to arrive at average illuintnance. A step-by-step explanation of the method plus illustrative examples will demenstrate the procedure. The reader should follow the steps with the flow chart in Fig. 20 38 and the calculation form in Fig. 20.39.

STEP 1. First, dimensional data are recorded, in others, schools, and many other occupancies

		Lamp Date	9	Lamo			1	1 000			
Abbroviation	LEUTD (W)	Diameter Length (in) (in)	Length (in)	Current	Ranas!	Total	Live (h)°	Output (Im)*	al 40%	Actual Ellicacy (Im/W)	Romarke
Preheat lamps									1		
F-15 T-8 CW	15	7.0	18	436	æ	2	2002 2	010			
F-20 T-12 WW	50	13'8	7.7	430	0	30	000 5	1 300	. 765	eg :	Cool white
Rapid-start-preheat lumber	cai lumo	z					2001	0001	00111	24	Warm white
F40 7-12 CW	4.0	12%	d)	400							
F40 T-12 WW	90	76.	27	900	0.7	40	20,000 +	3,150	12.770	69	
F40 T.19 CWY	2 3		00	430	7.5	46	20,000+	3,200	2.015	70	Warm white
CAL 21-10-1	06	**.	43	430	17	46	20,000+	2250	18.52	900	Cool while deliver
F40 1-12 D	40	13/3	48	430	7.5	46	20 000 +	2 600	000000	22	Cool writte peluxe
F40 T-12/C50	40	13%	48	430	7.5	97	20,000	2000	4.450	70.	Daylight
F40 T-12/C75	40	12%	du	630		10	00000	2,600	050'	07	5000 K color
FAD T.1241	70			00.	2.7	0	+0000	5,000	1,720	79	7500 K color
0.3	40	44.	1	430	4 7.5	4.5	12,000	2.900	2.525	55	"U" shape"
Rapid start-high	סחנשחו										2000
F48 T-12 CW/HO		13,8	0,3	600	19.5	70.5	40 000	000	-	,	
F60 T-12 CW/HO	75	.72.	0.00	BCO.	1,5	200	2000	000.	3,740	25	
F72 T-15 CW/HO	A.S.	12%		000		05.	2007	2.400	4.700	3	
011110	00	0	7,	900	22.5	107 5	12,000	6,550	5,785	62	
LAP 1-12 CW/HO	110	1/2	5	800	18.5	128.5	12,000	5.200	8.005	72	
Rapid-start-very h	high output	× 1110									
F48 PG-17 CW	110	167	u u	1500	4	100					
F72 PG. 17 CW	100		0 7 5	000		011	COO	6,900	2.150	55	G.E. Power Groove?
200000000000000000000000000000000000000	20.	0,	7	300	10	50	12,000	11,500	8.510	99	S.E. Power Grubve
Fab PG-17 CW	515	1,6;	96	1500)	01	225	12,000	0000'9:	12.160	7.1	wi
Insignt-start (Similine) lamps	ine) lamp	50									
F42 T.6 CW	25	6,3	42	200	10.5	35.5	7.500	1,750	1 200	40	
F64 T-6 CW	40	36	3	200	.7	49	2 500	2860	0 350	22	
F24 T.12 CW	50	. 20	PC	0.50	1.3	.)4.	2 535	1 150	200	7.0	
FAR T. 10 CW	S	12%	25	027			2000	0000	2000	5.	
EAD T. 12 CW	3 5	760	200	420	2 0	22	0000	00000	2000.	7	Warm while
10 11 10 11	2 1	44	0 1	107	77		3,000	3,000	5,750	28	
F72 T-12 CW	25	2.5	75	430	=	00	12,000	4,550	4.275	69	
F96 T-12 CW	75	9,21	96	430	13		12.000	6,300	1 5,800	74	
Data given for a preheat circuit	eat circuit				0 F.A.3	(minning 4-001 1944	(Kujum)				
Figures are for a two-lamp circuit	Jamp cut	hir			"Inch	achdes ballast loss.	ist loss.				
'ANSI ligures.					"Dat	diven in	Data given for langs in a rapid-start circuit.	a rabid-s	art Carbut		